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# MINIMIZING MEMORY EFFECTS IN OFDM TRANSMITTERS USING ADAPTIVE BASEBAND EQUALIZATION

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**Abstract** – This paper presents a simple and effective approach for eliminating memory effects in OFDM transmitters. It uses advantages of OFDM systems to provide pre-compensation of the frequency-dependent distortions, which are results of the power amplifiers (PA) memory effects. The process of memory effects quantification is carried out in this paper by obtaining a frequency-dependent PA gain, phase shift and intermodulation products. The memory effects are eliminated at baseband using equalization of the IDFT signal. Implementation of the equalization procedure at baseband makes the process of minimizing memory effects simple and effective, because no additional RF components or feedback loops are used. Memory effects are compensated in DSP part using simple multiplication of the frequency-domain digital signal by coefficients, which are calculated adaptively for each OFDM sub-carrier frequency and input power. The approach is tested with Motorola MOSFET MRF9742 power amplifier model in Advanced Design System (ADS). Simulations show significant improvement in minimizing memory effects. Received constellation of the 16-QAM OFDM signal after implementing baseband pre-compensation technique looks alike ideal one, whereas without pre-compensation it shows high dispersion due to the presence of PA memory.

## I. Introduction

The real characteristics of power amplifiers often differ from their polynomial models [5]-[6], [11]. This is caused by the dependence of PA output not only on the input but also on the previous input signals, called "Memory Effects" [11].

Memory effects are divided into electrical and thermal [6], [12]. Electrical memory effects appear because node impedances depend on frequency and there are several distortion sources in an amplifier. Therefore, distortion components produced by the different nodes have frequency-varying baseband, fundamental, second, third and other harmonics, which form the frequency-dependent behaviour of the amplifier. Thermal memory effects are caused by the fact that self-heating and environmental changes modify the temperature-dependent electrical characteristics of transistors. In other words, varying signal strength and environmental temperature causes thermal memory effects [6], [13].

Works [3], [6], and [13] show, that thermal memory affects low modulation frequencies and electrical memory influences the high-frequency performance. It means that the impact of thermal memory is more important for narrow-band systems. For wideband systems such as WiMax the main frequency-dependent distortion is caused by the electrical memory effects [13].

Current work aims to minimize memory effects in OFDM WiMax system. Therefore, advantages of OFDM system, such as IDFT, are used. Section 2 describes the process of quantifying memory effects in a real power amplifier system. It determines frequency-dependent gain and phase shift, which are used for calculating equalization function to minimize memory effects by digital operations with baseband IDFT signal. Section 3 describes the adaptive baseband equalization approach for minimizing memory effects in OFDM transmitters. It uses transistor-level model of a MOSFET power amplifier in ADS simulations for verification performances of the considered method.

## II. Quantifying Memory Effects

To quantify memory effects several methods have been proposed [3-6], [11-12]. Dependence of the magnitude and phase of intermodulation products IM3 on tone spacing as well as a gain dependence on the modulation frequency indicates the presence of memory. Distortion of a constellation diagram at the PA output when it operates in a linear mode is also a consequence of memory effects.

This paper presents a quantification and elimination of memory effects for a power amplifier using the developed baseband equalization approach. To demonstrate performance of the proposed method, ADS transistor-level model of a MOSFET power amplifier MRF9742 has been used for simulations. The current section presents results of MRF9742 simulations. It demonstrates presence of memory effects by a frequency-dependent gain, IMD and distorted constellation in a linear mode. Section 3 describes the proposed baseband equalization approach and verifies it by simulations.

Matlab-ADS co-simulation system has been used for simulations. Motorola MOSFET model showed on Fig. 1 was used as an active device in ADS analog circuit for a PA exhibiting memory effects. OFDM signal source was implemented in Matlab code and called from ADS. Such approach allows providing convenience and flexibility in generation any kind of input signal by using Matlab signal source, where desired equalization approach can be easily implemented.

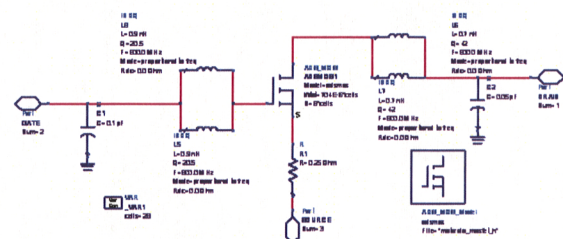


Figure 1. Motorola MOSFET model for ADS simulations

Results of the simulations are presented on Fig. 2-7. Fig. 2 shows gain dependence versus output power at different input frequencies for the investigated power amplifier. MRF9742 has a 12-dB gain and a 25-dBm compression point. In order to quantify only memory effects but not a saturation, the power range for further simulations has been chosen as  $P_{out} = 0 \dots 15$  dBm. The tone difference for two-tone tests was taken in range of 10 kHz – 30 MHz. Variation of the gain over frequency indicates presence of memory effects. This is more visually demonstrated on Fig. 3, where the gain versus frequency is presented. This distortion also depends on a power level. For  $P_{out} = 0$  dBm the gain is almost independent of the modulation frequency whereas for  $P_{out} = 15$  dBm it is significantly varying. In a memoryless amplifier there is no

phase change for the fundamental signal and intermodulation products IM3 [4]. Moreover, IM3 magnitude is proportional to the input power only and is independent of frequency. Therefore, varying phase and IM3 magnitude are often used to quantify memory effects [4]-[6].

Fig. 4 demonstrates a variation of the fundamental signal phase over modulation frequency due to memory effects.

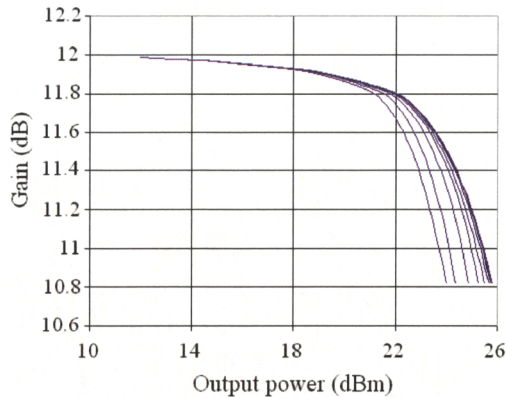


Figure 2. Simulated MRF9742 gain for different modulation frequencies (10 kHz - 30 MHz)

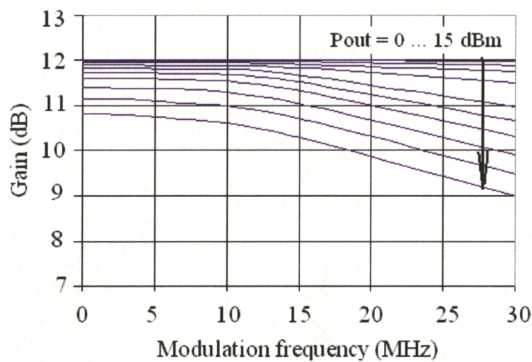


Figure 3. Simulated MRF9742 gain variation due to memory effects

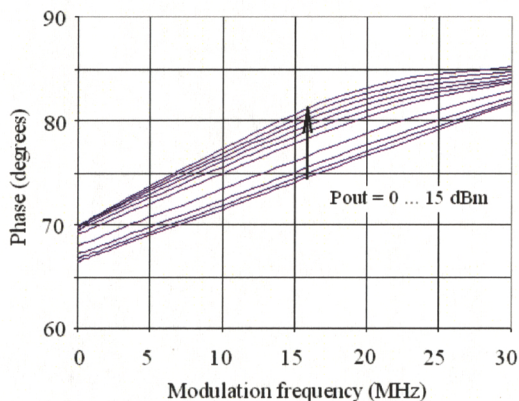


Figure 4. Simulated MRF9742 phase variation due to memory effects

3D-plots of the IM3 magnitude and phase are shown on Fig. 5 and Fig. 6 respectively. The variations over frequency indicate memory effects. Finally, a received con-

stellation for 16-QAM signal at  $P_{in} = -5$  dBm is presented on Fig. 7. The constellation is distorted due to memory effects because the power amplifier operates in a linear mode and all the other components are taken ideal.

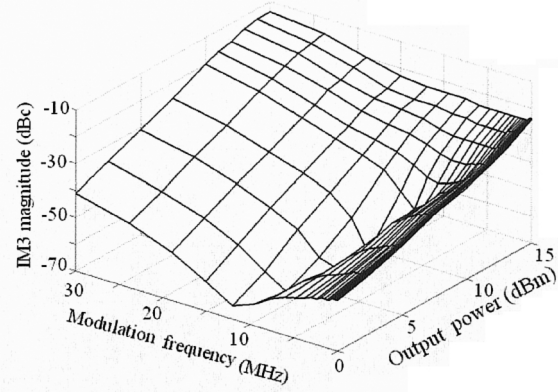


Figure 5. Simulated MRF9742 IM3 magnitude versus power and frequency

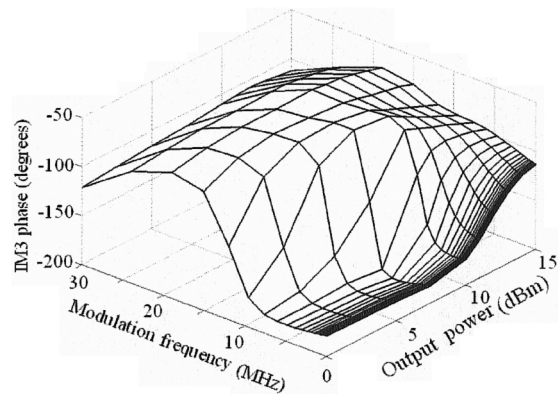


Figure 6. Simulated MRF9742 IM3 phase versus power and frequency

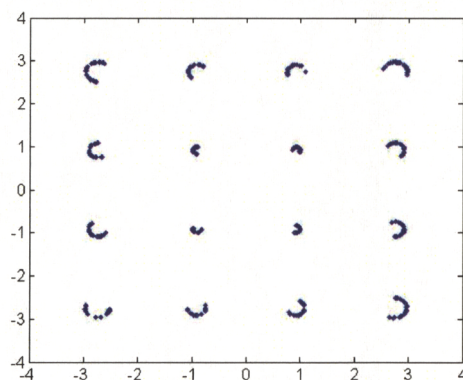


Figure 7. Received constellation distortion due to the memory effects ( $P_{in} = -5$  dBm)

### III. Baseband Equalization Method

Power amplifiers with memory effects are usually modelled by a filter and a non-linear element connected in series [1], [7-11]. If the filter precedes the non-linear block,



this is a Wiener model; otherwise it is a Hammerstein model. In this work a Wiener model for a power amplifier is considered (Fig. 8). The non-linear block is usually represented by the polynomial model described in [14]. The filter characterizes source of a frequency-dependent behaviour or memory effects. Therefore, to compensate for the memory effects it is necessary to analyze the filter. It has a frequency response which depends on the input power level  $H(f, P_{in})$ .

To compensate for the memory-related distortions, equalization is usually used. Advantages of OFDM signals such as IDFT allow to make this equalization at baseband by simply multiplying the IDFT inputs by  $1/H(f, P_{in})$  [2, 7, 8].

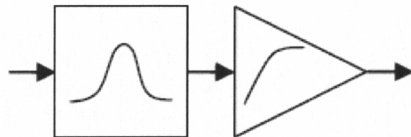


Figure 8. Wiener model for PA

There are several challenges in this approach, which need to be solved before implementing this method to a particular amplification system.

First of all,  $H(f, P_{in})$  should be normalized in order not to affect the mean power level.

Secondly, to make the equalization system adaptive to the input power level, the frequency response of the filter at all possible power values should be calculated and stored in an index table.

Then the frequency response  $H(f, P_{in})$ , corresponding to the input power level will be taken from the index table for pre-compensation. In the case of 16-QAM there are 4 possible levels of I and Q signals (-3, -1, 1, 3). As base-band power is proportional to  $I^2 + Q^2$ , there are 3 possible values of the input power corresponding to:  $1^2 + 1^2$ ,  $3^2 + 1^2$  and  $3^2 + 3^2$ . For the case of 64-QAM there are 8 levels for I and Q signals and therefore, 10 possible values for the input power. For those values frequency response of the filter should be tabulated.

For the case of considered MRF9742 power amplifier the process of baseband equalization is described below with an example of 16-QAM input signal.

The magnitude and phase of the normalized filter frequency response are extracted from the gain and phase curves for MRF9742 (Fig. 3, 4). The baseband signal levels chosen for the simulation are presented in Table I. At these levels, the amplifier exhibits memory effects, but it is not in saturation. As a 16-QAM input is considered, baseband signal has 3 possible magnitude values (Tab. I).

The WiMax 64-OFDM 16-QAM system is used. For baseband power  $P_{bb} = -20.8$  dBm,  $-6.8$  dBm and  $-1.7$  dBm the normalized complex values  $H_{norm}(f, P_{in})$  are calculated using the obtained gain and phase dependences (Fig. 3, 4). Magnitude and phase of the normalized frequency response for the considered 16-QAM modulation are presented on Fig. 9, 10 respectively.

To compensate for the memory effects, the complex baseband signal was multiplied by  $1/H_{norm}(f, P_{in})$ . After that, IDFT was performed and an OFDM waveform was created. It passed MRF9742 amplifier at a mean input power level of  $-5$  dBm. The received constellation was obtained (Fig. 11). Comparing with the constellation at Fig. 24, dispersion due to the memory effects is almost eliminated, which characterizes that the frequency response  $H_{norm}(f, P_{in})$  is calculated accurately and the baseband equalization is performed correctly.

TABLE I  
Voltage and Power Levels for Simulations

$mag(I)$ , V	$mag(Q)$ , V	$mag(V_{bb})$ , V	$mag(P_{bb})$ , dBm
0.12	0.12	0.03	-20.81
0.12	0.36	0.14	-6.83
0.36	0.36	0.26	-1.73

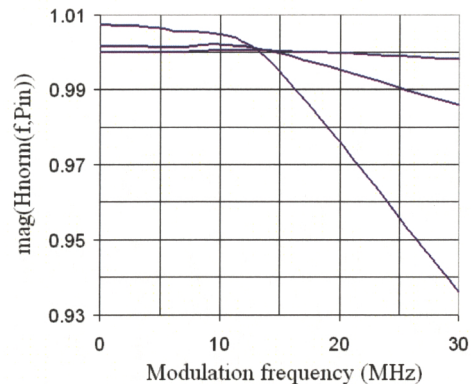


Figure 9. Magnitude of the normalized frequency response  $H_{norm}(f, P_{in})$  for 3 power levels of 16-QAM

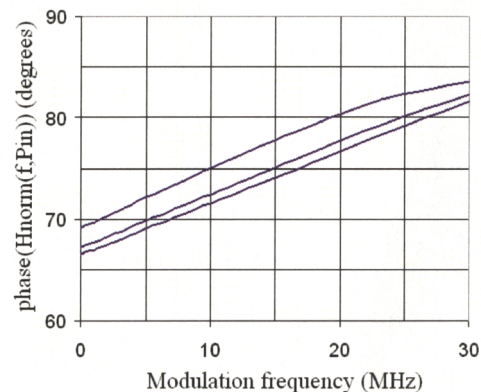


Figure 10. Phase of the normalized frequency response  $H_{norm}(f, P_{in})$  for 3 power levels of 16-QAM

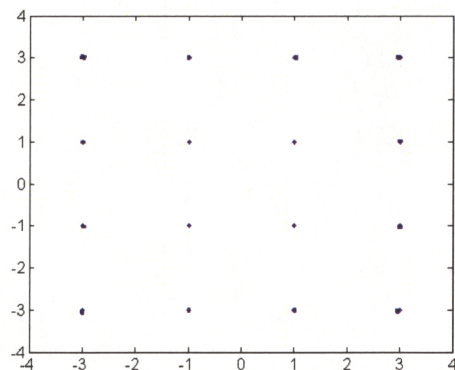


Figure 11. Simulated received constellation for MRF9742 using baseband equalization ( $P_{in} = -5$  dBm)

## IV. Conclusion

A baseband equalization approach for minimizing memory effects has been presented in this paper. It uses digital pre-compensation of the input signal at baseband before IDFT in OFDM waveform. The proposed method was verified by Matlab-ADS co-simulation of the transceiver based on Motorola MOSFET MRF9742 active device. Simulation results proved good performance of the method in eliminating memory effect of the power amplifier. Quantification of the memory effects was performed by obtaining frequency-dependent gain, phase and IM3 performances of the PA. It was shown, that memory effects have high influence on the dispersion of the received constellation. After implementing proposed approach, significant improvement in received constellation for the same power level has been achieved. The baseband equalization method is a simple, low-cost, easily implemented technique, which is performed at DSP part and does not require additional components or hardware change in RF part. Described advantages make the method favourable for minimizing memory effects in OFDM systems.

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## МИНИМИЗАЦИЯ ЭФФЕКТОВ ПАМЯТИ В ПЕРЕДАТЧИКАХ OFDM ПУТЕМ АДАПТИВНОГО ВЫРАВНИВАНИЯ ПО ЧАСТОТЕ МОДУЛИРУЮЩЕГО СИГНАЛА

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**Аннотация** – Данная статья описывает простой и эффективный подход для устранения эффектов памяти в передатчиках OFDM. Преимущества ортогональной частотной модуляции используются для прекомпенсации частотно зависимых искажений, являющихся результатом эффектов памяти в усилителях мощности. Процесс количественной оценки эффектов памяти выполнен в статье путем получения частотно зависимых характеристик усиления, фазового сдвига и интермодуляционных продуктов. Эффекты памяти устраняются с помощью частотного выравнивания дискретного ОПФ модулирующего сигнала. Реализация процедуры на уровне модулирующего сигнала упрощает и делает более эффективным процесс устранения эффектов памяти, поскольку не используются дополнительные РЧ компоненты и цепи обратной связи. В блоке ЦОС производится простое умножение в частотной области сигналов на коэффициенты, которые адаптивно рассчитываются для каждого значения частоты и входной мощности вспомогательной несущей OFDM. Предложенный метод протестирован на модели усилителя мощности компании Motorola, построенного на полевом транзисторе с МОП-структурой MRF9742 в программе ADS. Результаты моделирования показали существенное уменьшение эффектов памяти. После внедрения метода частотного выравнивания модулирующего сигнала вид принятой звездной диаграммы сигнала 16-QAM OFDM близок к идеальному, в то время как без примени данного метода наблюдается значительное рассеивание звездной диаграммы из-за наличия эффектов памяти.